

Study of a single-phase series active power filter with hysteresis control

Mihail Hr. Antchev,
Mariya P. Petkova,
Hristo M. Antchev

Department of Power Electronics
Technical University - Sofia
Sofia, Bulgaria
antchev@tu-sofia.bg

Vanjo T. Gourgoulitsov
Power Engineering and Electronics College
at the Technical University – Sofia, Bulgaria
vtg_otk@abv.bg

Stanimir S. Valtchev
Department of Electrical Engineering and UNINOVA
Research Center, Faculty of Science and Technology,
Universidade Nova de Lisboa, Portugal
ssv@fct.unl.pt

Abstract— This paper presents results from a study of an active single-phase series power filter with a control system based on modified hysteresis method. Waveforms from the computer simulation and waveforms from the carried out tests of the filter are presented, comparing the operation at limited and unlimited maximum switching frequency of the power switches.

Keywords— series active power filter; hysteresis control; frequency limitation

I. INTRODUCTION

Active power filters (APF) are perspective means to improve the quality of the electrical energy [1,2]. Series active power filters are applied meanly to remove disturbances in the quality of the voltage of AC distribution network [3,4,5,6]. The most widely used topology of the single-phase filters power circuit is the full-bridge shown in Fig.1. The control of APF is carried out in such a way that in each moment the voltage U_F is added to the voltage of the grid U_S and produces the voltage that supplies the load U_L which has a waveform much closer to the sine wave. The filter L_F, C_F eliminates the harmonics in the filter voltage due to the high frequency switching. The transformer ratio of Tr depends on the value of the DC supply voltage. The control implementations may be different: pulse-width modulation, predictive control, sliding mode control, etc. [7,8,9]. Some control systems implementations have a constant switching frequency [10], some are based on hysteresis control with limitation of the maximum switching frequency. This last method shown in [11] allows optimizing the active power losses in the switches, and optimizing the design of the filter L_F, C_F , thus improving the electromagnetic compatibility of the converter as well.

The aim of the authors is to investigate the operation of the series APF shown in Fig.1 when its control system is implemented using hysteresis control with and without

limitation of the maximum switching frequency of the power devices.

II. OPERATIONAL BASIS

The control system of this APF is based on the comparison of the instantaneous values of a reference sine wave U_{REF} synthesized in phase with the grid voltage U_S to the load voltage U_L . The comparison is performed with a defined hysteresis voltage interval H . If the instantaneous value of the load voltage is lower than that of the reference sine wave, the transistors $VS1, VS3$ turn on, in case it is higher, then $VS2, VS4$ turn on. The reference sinusoid is generated through observing the voltage of the point of common coupling (PCC) U_S . If the reference sinusoid value is kept equal to that of the first harmonic of the U_S then only a filtering is carried out. If the reference sinusoid is maintained at constant amplitude then in addition to the filtering, a stabilizing of the voltage U_L is performed.

A. Hysteresis control without limitation of the maximum frequency

Fig.2 illustrates the concept of the implementation of the hysteresis control with no limitation of the maximum switching frequency. The turning on of the power switches happens when the above mentioned difference between U_S and U_L reaches values: $U_{REF} - H$ for $VS1, VS3$ and $U_{REF} + H$ for $VS2, VS4$.

The switching frequency of the power switches varies during the time of each half-period of the reference voltage and the maximum value of that frequency is theoretically unlimited. This value is possible to be changed by changing the hysteresis value H .

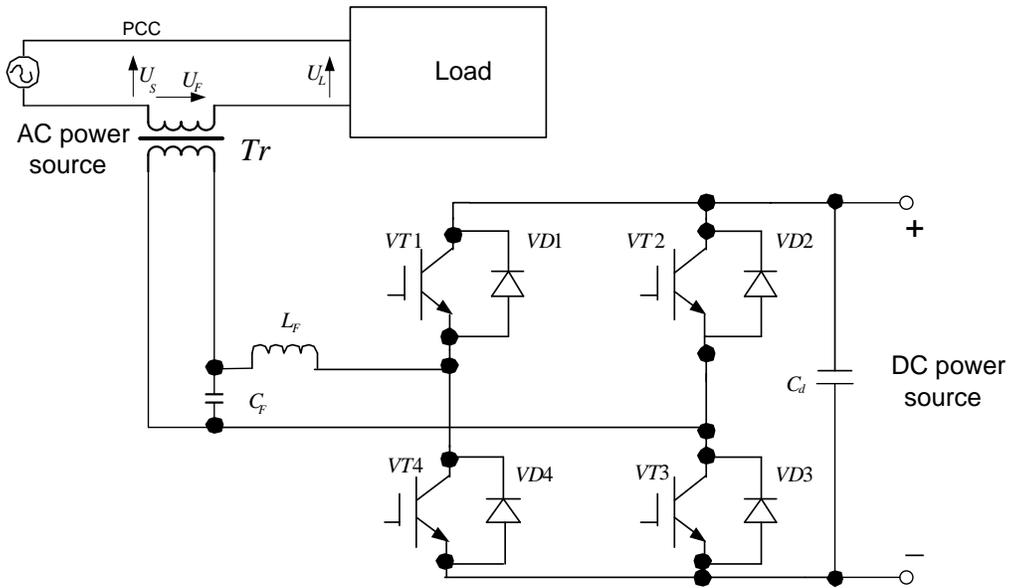


Figure 1. Power stage of a single-phase full-bridge series active power filter

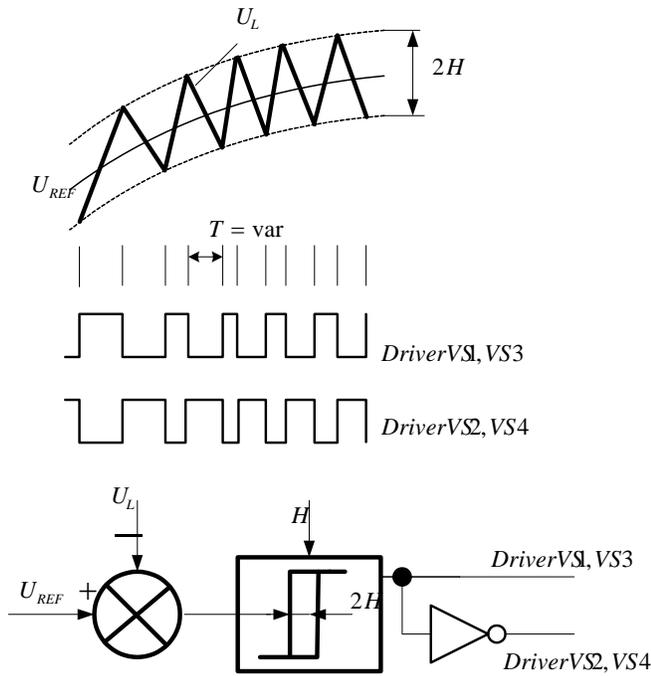


Figure 2. Building blocks and time diagrams illustrating the tracking down of the reference curve at a not limited maximum switching frequency

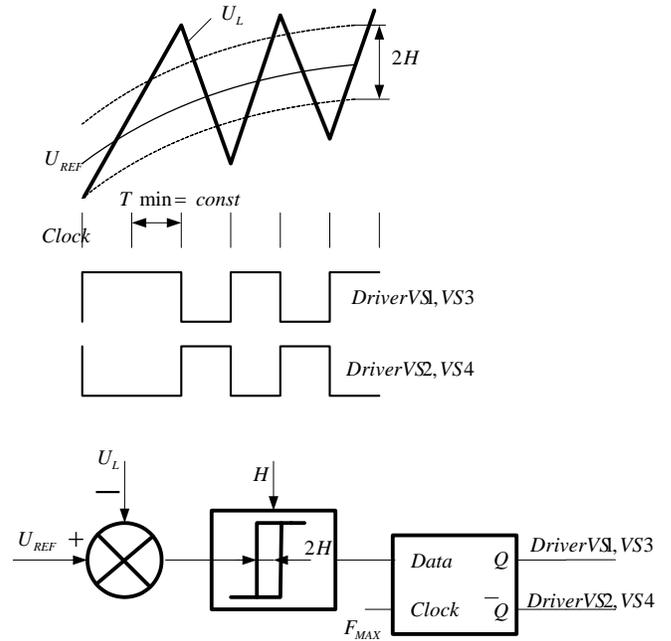


Figure 3. Blocks and time diagrams illustrating the tracking down of the reference curve at a limited maximum of the switching frequency

B. Hysteresis control at limited maximum switching frequency

Fig.3 illustrates the concept of the implementation of the hysteresis control with an imposed limitation of the maximum switching frequency. The turning on of the power switches does not happen immediately at reaching the value $U_{REF} - H$ for VS1, VS3 and the value $U_{REF} + H$ for VS2, VS4. The turning on is performed after arriving at the corresponding

values and delayed synchronously by the length of a clock signal. The frequency F_{MAX} of that signal will limit the maximum switching frequency of the power switches.

Using this control, a certain distortion of the sine wave is expected to be observed, instead of the ideal reference, but the positive result is the convenient more efficient operation of the power switches at this limited switching frequency.

III. COMPUTER SIMULATION

The simulation software applied was PSIM and the performed the computer simulation is relayed in the next figures.

A. Results from computer simulation without limitation of the maximum frequency

The operation of the single-phase APF is studied at a trapezoidal waveform of the grid AC voltage U_S . The considered here waveform is similar to that of a source with

limited power, loaded with a non-linear load – uncontrolled full wave rectifier with active-capacitive type of load without applying of power factor correction (PFC). Fig.4 displays the simulated (idealized) circuit for the computer simulation. The results of the simulation are shown in Fig.5, Fig.6 and Fig.7. The total harmonic content of the source voltage is estimated as high as 20%. The height (amplitude value) of the trapezoid is 300V. The values of the load resistance and load inductance are 400Ω and $2.4H$, respectively.

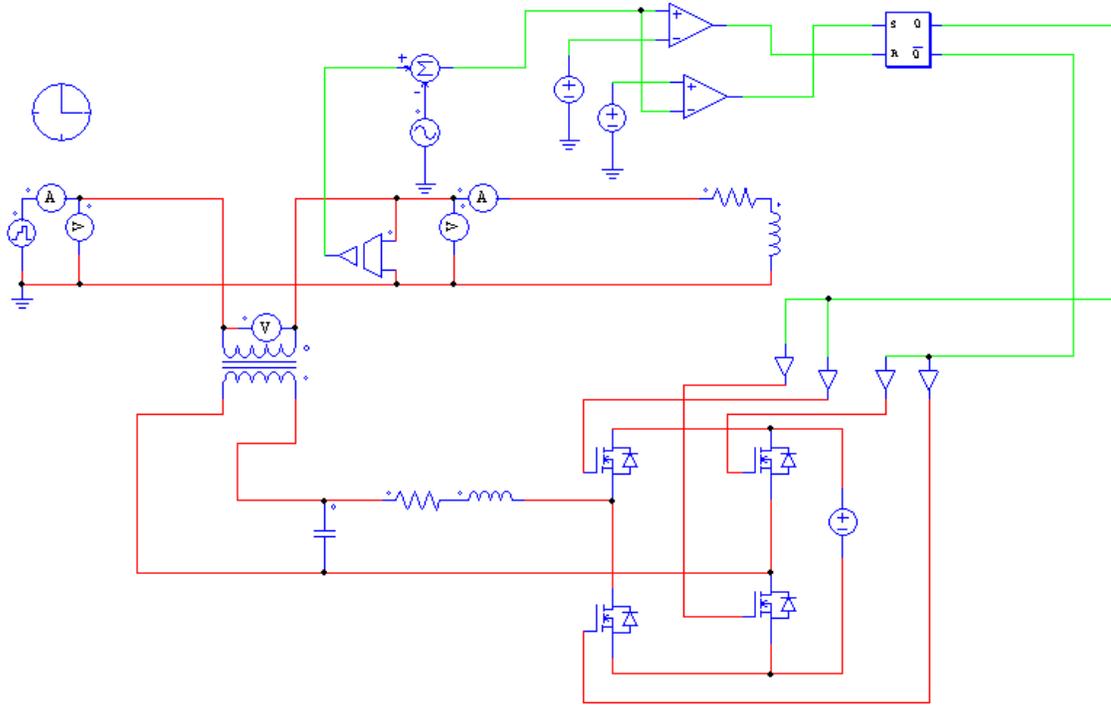


Figure 4. Idealized power stage and control circuits used for the computer simulation of the single-phase APF, when no limitation on the maximum switching frequency is applied and the load is complex, resistive and inductive (series connection)

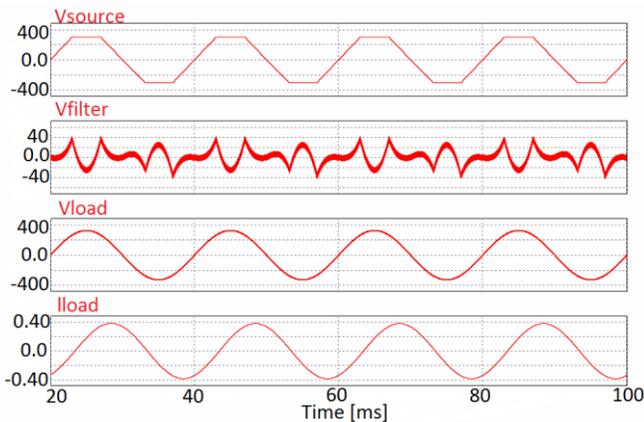


Figure 5. Results from the simulation of the circuit shown in Fig.4. From top to bottom: the grid voltage, filter voltage, load voltage and grid current, respectively. The time span is 80 ms

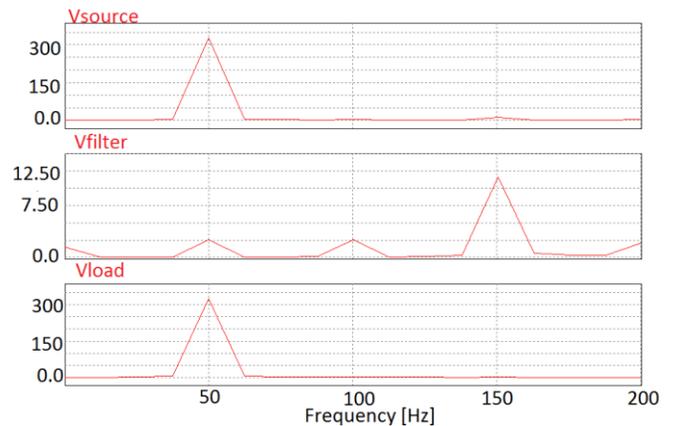


Figure 6. Harmonic spectrum from top to bottom :the grid voltage, filter voltage, load voltage, respectively. The range of X-axis is [0, 200 Hz]

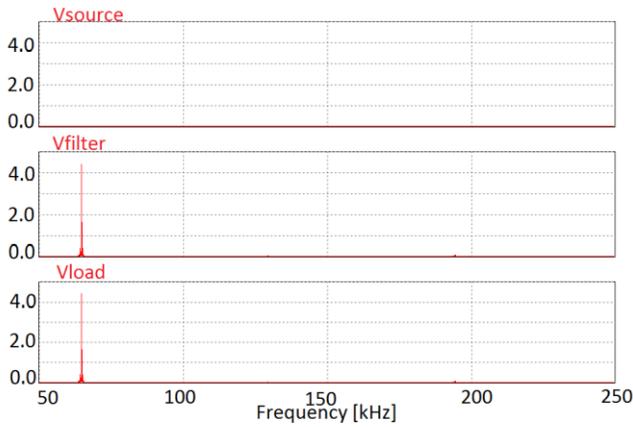


Figure 7. Harmonic spectrum from top to bottom: the source (grid) voltage, filter voltage, load voltage, respectively. The frequency span of the horizontal axis is from 50 kHz to 250kHz

B. Results from the computer simulations when the maximum switching frequency was limited

Fig.8 displays the computer simulation (idealized) circuit. The results of the simulation are shown in Fig.9, Fig.10 and Fig.11. The waveform of the AC (grid) source as well as the character and complex value of the load remain the same as in the previous case (unlimited switching frequency).

Comparing the results shown in Fig.7 and Fig.11, the main disadvantage of the operation at limited switching frequency is observed in the presence of some (not so many) higher order harmonics in the waveform of the load voltage with a broad spectrum.

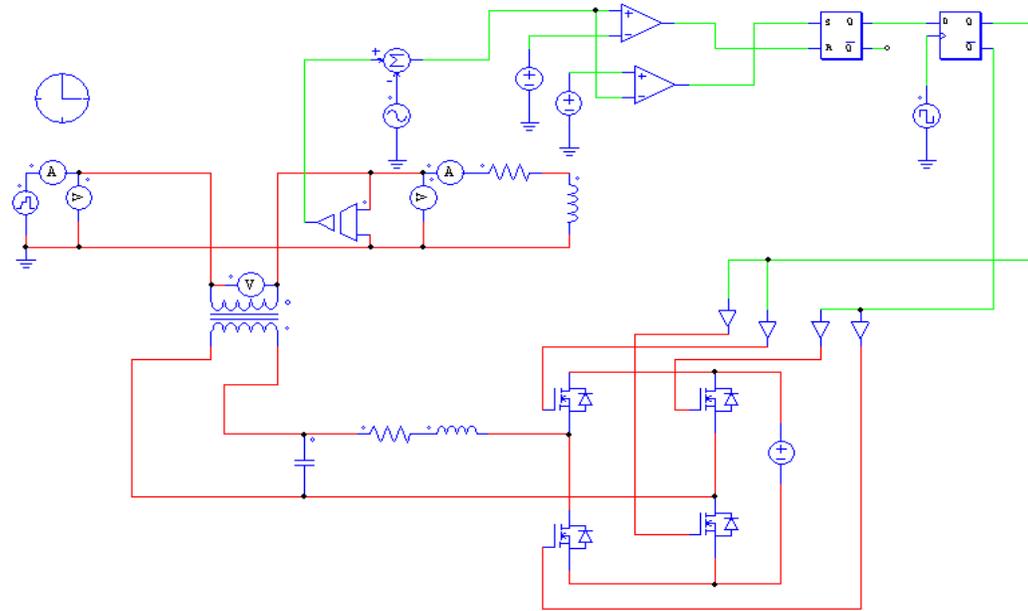


Figure 8. Idealized power stage and control circuits used for the computer simulation of the single-phase APF, when the limitation on the maximum switching frequency is applied and the load is complex, resistive and inductive (series connection)

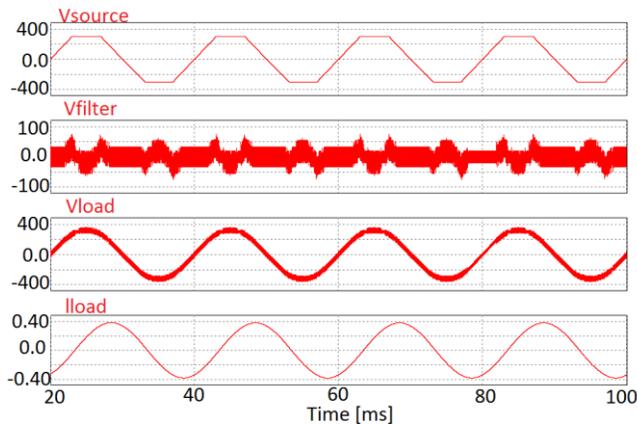


Figure 9. Results from the simulation of the circuit shown in Fig.8 when the switching frequency is limited to $f = 200kHz$. From top to bottom: the grid voltage, filter voltage, load voltage and source current

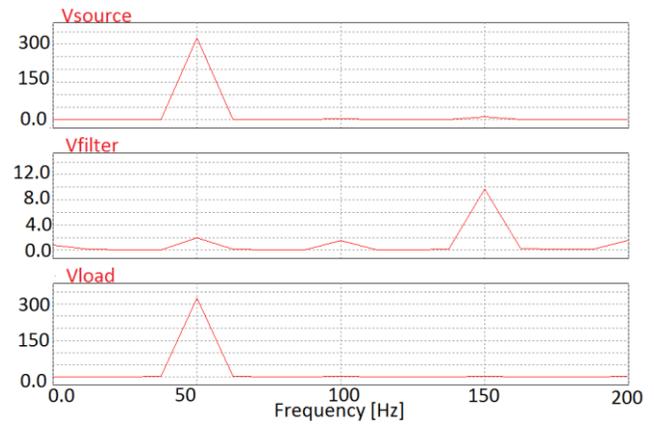


Figure 10. Harmonic spectrum from top to bottom: the grid voltage, filter voltage, load voltage, respectively. The horizontal axis range is from 0 to 200 Hz

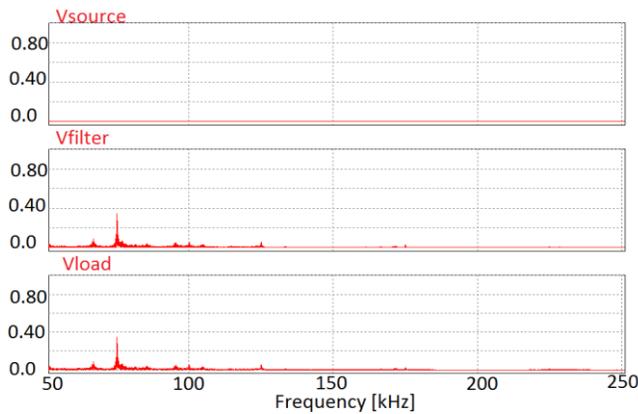


Figure 11. Harmonic spectrum from top to bottom: the grid voltage, filter voltage, load voltage, respectively. The X-axis range is 50 kHz to 250kHz

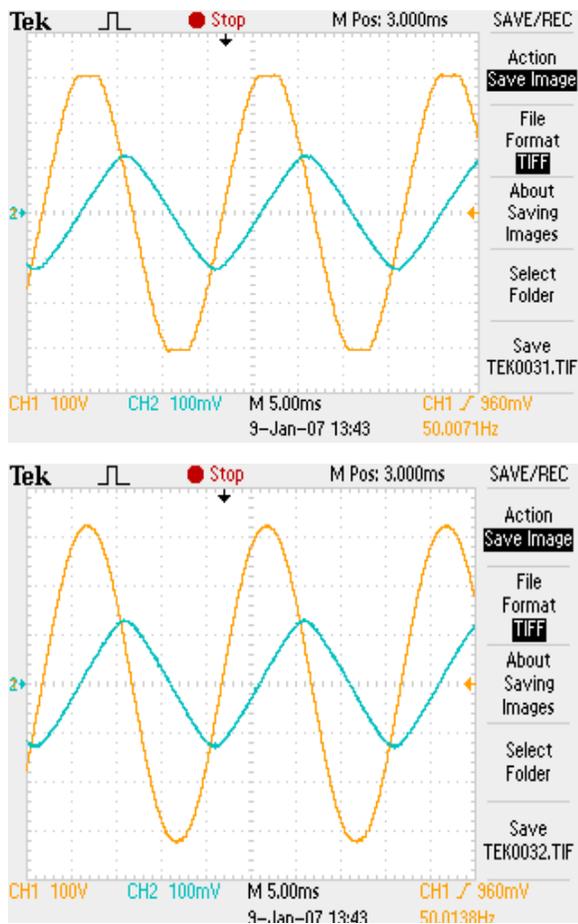


Figure 12. Experimental results of the operation of the single-phase series APF with active-inductive load CH1 – load voltage and CH2 – load current. Top – APF is off, Bottom – APF is on (no frequency limitation)

IV. EXPERIMENTAL RESULTS

Fig.12 displays the experimental results of the load voltage and current when the APF is off and on. The values of the load elements are the same as those used in the computer simulation. The APF is controlled using hysteresis control without frequency limitation.

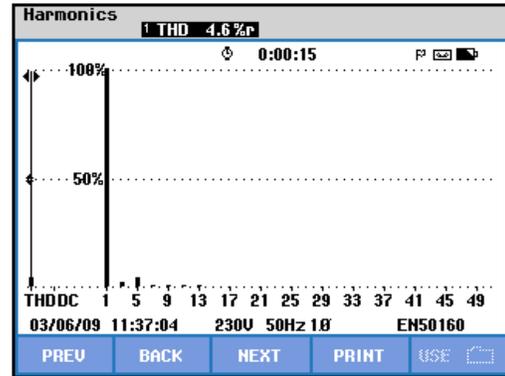
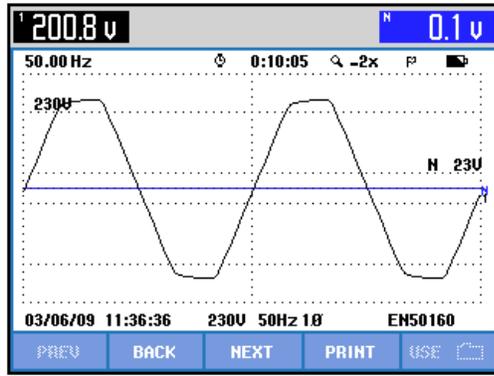
Fig.13 and fig.14 displays parameters of the load voltage, especially the harmonic spectrum and total harmonic distortion (THD) in both cases: with and without active power filtering (APF). In the case of the applied APF, the THD is reduced to 1.6%.

V. CONCLUSION

The hysteresis control methods studied (limited and unlimited switching frequency) of the single-phase active power filter are both performing well to achieve the general purpose: to eliminate the low order harmonics of the source (grid) voltage. A slight disadvantage of the limited maximum switching frequency is the presence of high order harmonics with a broad spectrum in the waveform of the load voltage.

REFERENCES

- [1] Akagi H. (2006). Modern active filters and traditional passive filters. Bulletin of the Polish Academy of Sciences, Technical Sciences, vol. 54, No 3, 2006.
- [2] Chiasson J. N., L. M. Tolbert, K. J. McKenzie and Z. Du, "A Complete Solution to the Harmonic Elimination Problem", IEEE Trans. On Power Electr., Vol.19, No. 2, pp.491-499, March, 2004.
- [3] Barrero F., S. Martinez, F. Yeves and P.M. Martinez, "Active Power Filters for Line Conditioning: a Critical Evaluation", IEEE Trans. On Power Delivery, Vol. 15, No. 1, pp.319-325, January 2000.
- [4] Fujita H. and H. Akagi, "The Unified Power Quality Conditioner: The Integration of Series- and Shunt- Active Filters", IEEE Trans. On Power Electr., Vol.13, No.2, pp.315-322, March 1998.
- [5] Ribeiro E., R. and I. Barbi. Harmonic Voltage Reduction Using a Series Active Filter Under Different Load Conditions. IEEE Trans.on Power Electronics, vol. 21, No 5, 2006, pp.1394-1402.
- [6] Srianthumrong S., H. Fujita, and H. Akagi, "Stability Analysis of a Series Active Power Filter Integrated with a Double-Series Diode Rectifier", IEEE Trans. On Power Electr., Vol.17, .No.1, pp.117-124, January 2002
- [7] Marks J.H., and T.C. Green, "Predictive Transient – Following Control of Shunt and Series Active Power Filters", IEEE Trans. On Power Electr., Vol.17, .No.4, pp.574-584, July 2002.
- [8] Petkova M.P., M.H.Antchev, V. T. Gourgoultsov, Investigation of single phase inverter and single phase series active power filter with sliding mode control, Chapter 2 in "Sliding mode control" edited by A.Bartoszewicz, INTECH, 2011,pp.25-44.
- [9] Wu W.M., L.Q.Tong, M.Y. Li, Z.M.Qian, Z.Y. Lu and F.Z. Peng, "A New Control Strategy for Series Type Active Power Filter", 35 th Annual PESC , Aachen, Germany, 2004, pp. 3054 - 3059.
- [10] Zhou L. and K. M. Smedley, "Unified Constant-Frequency Integration Control of Active Power Filters", APEC 2000, USA, New Orleans, 2000.
- [11] Antchev M.H., M.P. Petkova, A.T. Kostov, Hysteresis - current control of single - phase shunt active power filter using frequency limitation, conf. PES 2007, Cleanwater, USA, Proc., pp. 234-238.



HARMONICS TABLE

Volt	L1	N
THD%	4.5	97.9
H3%	1.8	0.9
H5%	3.9	0.9
H7%	1.0	0.9
H9%	0.4	0.9
H11%	0.6	0.9
H13%	0.6	0.8
H15%	0.3	0.9

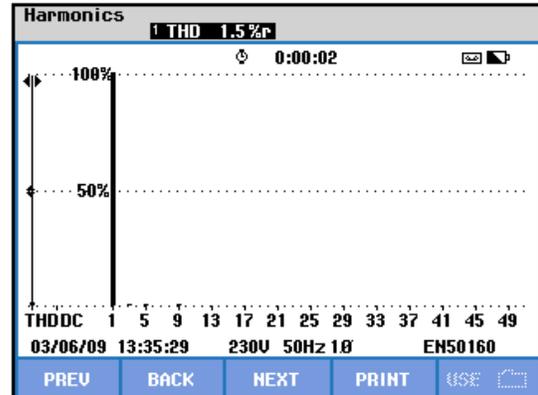
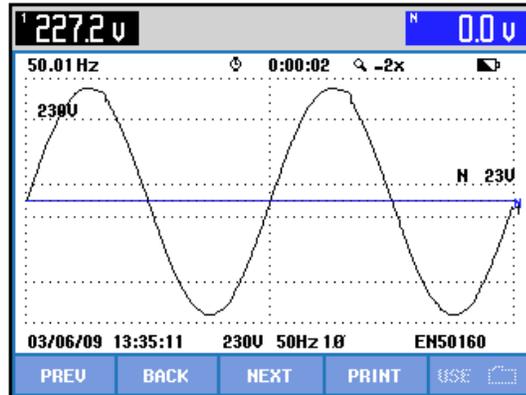
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HARMONICS TABLE

Volt	L1	N
THD%	4.5	98.4
H17%	0.2	0.8
H19%	0.1	0.9
H21%	0.1	0.9
H23%	0.1	0.8
H25%	0.0	0.8
H27%	0.1	0.9
H29%	0.0	0.8

03/06/09 11:53:40 230V 50Hz 1Ø EN50160

Figure 13. Parameters of load voltage when APF does not operate



HARMONICS TABLE

Volt	L1	N
THD%	1.6	98.5
H3%	0.9	2.7
H5%	0.7	2.0
H7%	0.3	2.2
H9%	0.4	2.6
H11%	0.4	2.2
H13%	0.3	2.3
H15%	0.2	2.1

03/06/09 13:36:56 230V 50Hz 1Ø EN50160

HARMONICS TABLE

Volt	L1	N
THD%	1.6	99.0
H17%	0.2	1.4
H19%	0.1	1.2
H21%	0.1	1.4
H23%	0.1	1.2
H25%	0.0	1.2
H27%	0.1	1.2
H29%	0.1	1.2

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Figure 14. Parameters of load voltage when APF operates