# INVESTIGATION ON EROSIVE WEAR OF BIODEGRADABLE THERMOPLASTIC POLYMER SAMPLES PRODUCED BY 3D PRINTING

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### ABSTRACT

The present paper presents the results of a study of tribological characteristics of biodegradable thermoplastic samples produced by FFF/FDM 3D printing subjected to erosive wear. The samples are printed at five different nozzle temperatures (190 °C, 200 °C, 210 °C, 220 °C and 230 °C). Results about mass wear, wear intensity, wear resistance, roughness and microhardness of the different samples are obtained.

Keywords: biodegradable polymers, erosive wear, 3D printing, tribology.

#### AIMS AND BACKGROUND

Polylactic acid (PLA) is a biodegradable thermoplastic polymer produced by condensation polymerisation of lactic acid, which is derived by fermentation of sugars from carbohydrate sources<sup>1</sup>. This polymer is becoming more and more popular in various fields<sup>2</sup> – industry, medicine, art, etc.<sup>3,4</sup>, mainly because the material could be printed on budget 3D printers, it is not toxic, it has a low thermal expansion that helps reduce the internal stresses caused during cooling down and the polymer is biodegradable under specific conditions<sup>5,6,7,8</sup>. These applications require a better understanding of its mechanical and tribological properties.

The erosive wear of machine parts is a process of surface destruction under the impact of solid or liquid particles carried by a fluid flow - air, water, oil, etc. It is one of the most dangerous types of wear because it leads to a rapid deterioration of the functional characteristics of the machines in general and to a reduction of their resource. This is associated with huge costs for materials, spare parts, consumables and human resources for maintenance in the operation process. The other side of the problem is related to environmental pollution and the increasing extraction of raw materials from nature, which is directly related to the balance in the ecosystems<sup>9,10</sup>.

The aim of the current study is to investigate and to analyse mass wear, wear intensity, wear resistance, microhardness and roughness of PLA samples 3D printed at different nozzle temperatures in condition of erosive wear.

#### EXPERIMENTAL

For the purposes of the study five types of PLA samples are printed using FDM/FFF technology. The samples are printed on Anycubic Mega S 3D printer at five different nozzle temperatures: 190°C (sample PLA-190TE), 200°C (sample PLA-200TE), 210°C (sample PLA-210TE), 220°C (sample PLA-220TE) and 230°C (sample PLA-230TE). Some basic process parameters are presented in Table 1.

Parameter	Value	Unit
Layer Height	0.2	mm
Line Width	0.4	mm
Infill Density	100	%
Infill Pattern	Grid	-
Build Plate Temperature	60	°C
Print Speed	50	mm/s
Initial Layer Print Speed	25	mm/s
Fan Speed	100	%
Build Plate Adhesion Type	Skirt	-
Infill Overlap percentage	15	%
Skin Overlap percentage	5	%

Table 1. Basic process parameters of 3D printing

The erosion wear of the studied samples has been accomplished by means of air stream, carrying abrasive particles in atmospheric environment. The functional scheme of the device is represented on Fig. 1. The designation of this device is to produce bi-phase jet «air-abrasive particles» by independent setting and regulation of the parameters of the two separate stationary flows – air flow and abrasive mass flow and more specifically – the air pressure and the flow rate of the abrasive particles<sup>11</sup>.



- 1 chamber for solid particles
- 2 mixing chamber
- 3 chamber with manometer
- 4 sample
- 5 holder
- 6 regulator

Fig.1. Scheme of erosive wear test device

The corresponding formulas are presented in Table 2.

Table	<b>2.</b> I	Form	ulas
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Doromotor	Mass	Mass erosion	Erosion	Erosion	Erosion wear	Relative wear
Farameter	flow rate	wear	rate	intensity	resistance	resistance
Formula	$\dot{m}_a = \frac{m_a}{t_a}$	$m_{\rm e}=m_{\rm e}^0-m_{\rm e}^i$	$\dot{m}_e = \frac{m_e}{\Delta t}$	$i_e = \frac{\dot{m}_e}{\dot{m}_a}$	$I_e = \frac{1}{i_e}$	$R^e_{i,j} \!\!=\!\! \frac{I^e_i}{I^e_j}$

The parameters of the erosive wear experiment are presented in Table 3.

Parameter	Value
Solid particles material	silicon dioxide
Maximum size of the particles	600 µm
Air stream pressure	0.1 MPa
Particles flow	175.6 g/min
Impact angle of the particles	90°
Distance between the sample and the nozzle	10 mm
Duration of the test	5 minutes
Ambient temperature	22°C

Table 3. Parameters of the erosive wear experiment

The mass of the samples is measured with electronic scale WPS-180/C/ with accuracy of 0.1 mg. Before each measurement the sample is cleaned using a solution, neutralizing the static electric charge, and then it is dried up.

Microhardness and roughness are also investigated. The microhardness is measured before and after wear with HVS-1000 microhardness tester using Vickers hardness scale (Fig. 2). The load is set to 0.5 kg and the holding time is set to 10 s. The roughness is measured before and after wear with Tesa Rugosurf 20 roughness gauge (Fig. 3).





Fig. 2. Measuring of the microhardness after wear Fig. 3. Measuring of the roughness after wear

## **RESULTS AND DISCUSSION**

Results for various characteristics of erosive wear are presented in Table 4.

Sample	Mass wear,	Erosion rate,	Intensity	Erosion wear	Relative erosion
Sample	mg	mg/min	of erosion	resistance	wear resistance
PLA-190TE	1.8	0.36	2.05 x 10 <sup>-6</sup>	0.49 x 10 <sup>6</sup>	1
PLA-200TE	1.7	0.34	1.90 x 10 <sup>-6</sup>	0.53 x 10 <sup>6</sup>	1.08
PLA-210TE	1.5	0.30	1.70 x 10 <sup>-6</sup>	0.59 x 10 <sup>6</sup>	1,2
PLA-220TE	0.7	0.14	0.80 x 10 <sup>-6</sup>	1.25 x 10 <sup>6</sup>	2.6
PLA-230TE	0.5	0.10	0.57 x 10 <sup>-6</sup>	1.75 x 10 <sup>6</sup>	3.6

Table 4. Results for various characteristics of erosive wear

A graphical representation of the dependence of the erosion intensity on the printing temperature is shown on Fig. 4.





Graphical representations of the erosion wear resistance and relative erosion wear resistance for the different samples are presented respectively on Fig. 5 and Fig. 6.





Fig. 6. Relative erosion wear resistance

The microhardness values before and after erosive wear are presented in Table 5.

Table 5. Where the area shown and area crossive wear	Table	5.	Μ	icro	harc	lness	values	before	and	after	erosive	wear
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Sample	Initial hardness (HV)	Hardness after erosion (HV)
PLA-190TE	19.06	35.9
PLA-200TE	18.20	37.2
PLA-210TE	17.50	36.7
PLA-220TE	17.90	36.5
PLA-230TE	17.70	39.3

The roughness values before and after erosive wear are presented in Table 6.

Sample	Initial roughness (Ra)	Roughness after erosion (Ra)
PLA-190TE	2.112	4.32
PLA-200TE	2.792	4.42
PLA-210TE	2.677	4.16
PLA-220TE	2.597	3.91
PLA-230TE	1.808	4.07

Table 6. Roughness values before and after erosive wear

The present results that in case of producing parts such as fans, fins, etc. – elements that are subjected to erosive wear in the course of exploitation, it is important to choose the highest possible printing temperature.

### CONCLUSIONS

The obtained results show that with increasing of the printing temperature, the intensity of erosion decreases non-linearly in the range from  $210^{\circ}$ C to  $230^{\circ}$ C. At lower printing temperatures ( $190^{\circ}$ C and  $200^{\circ}$ C) the intensity of erosion changes slightly. It is found that the sample produced at the highest printing temperature ( $230^{\circ}$ C) has the highest erosion wear resistance – 3.6 times higher than the wear resistance of the sample printed at  $190^{\circ}$ C. In summary, it can be stated that an increase in printing temperature by  $40^{\circ}$ C leads to an increase in wear resistance by 360%.

Microhardness studies show a definite tendency for a double increase in microhardness after erosion wear compared to the initial values of the parameter.

The roughness values after erosive wear show a two-fold increase compared to the initial values.

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